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***Communication Systems***

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**Narrowband Frequency Modulation:**

Consider equation above,

$$s(t) = A_c \cos(2\pi f_c t + \beta \sin(2\pi f_m t)) = \\ A_c \cos 2\pi f_c t \cdot \cos(\beta \sin(2\pi f_m t)) - A_c \sin 2\pi f_c t \cdot \sin(\beta \sin(2\pi f_m t))$$

$\beta$  is small compared to one radian, we may approximate

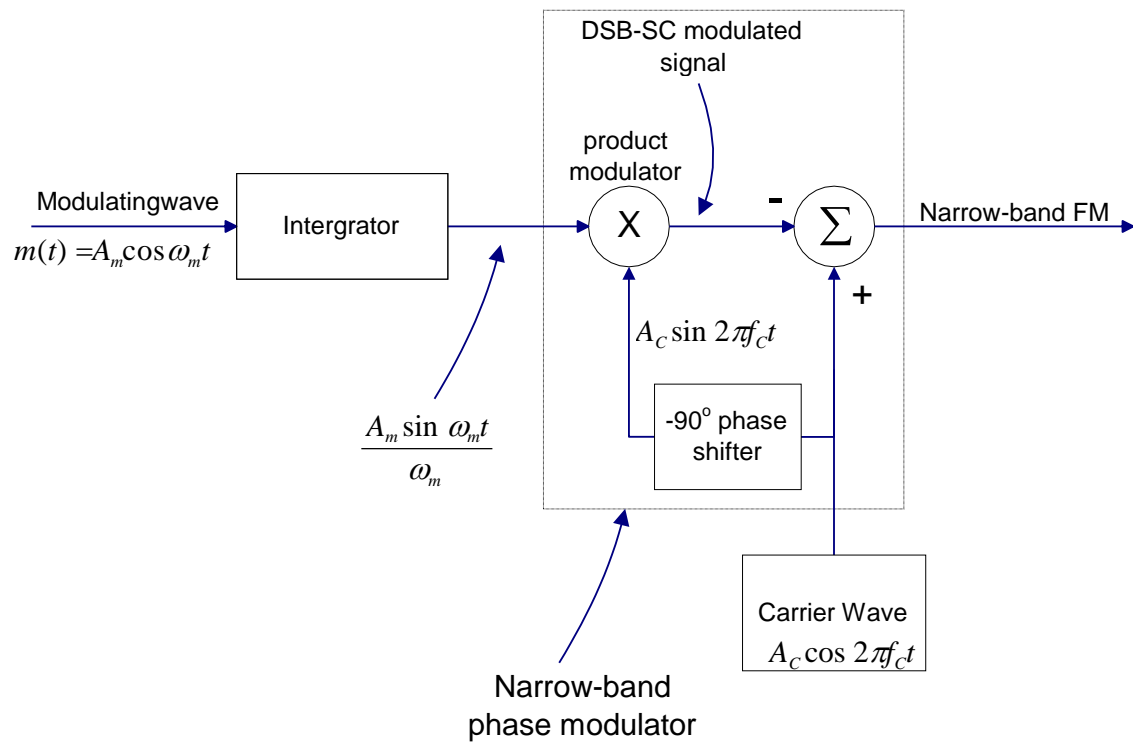
$$\cos(\beta \sin 2\pi f_m t) \approx 1 \\ \text{and} \\ \sin(\beta \sin(2\pi f_m t)) \approx \beta \sin(2\pi f_m t)$$

Hence equation 2.18 becomes

$$s(t) \approx A_c \cos(2\pi f_c t) - \beta A_c \sin(2\pi f_c t) \cdot \sin(2\pi f_m t)$$

↑  
*Narrowband FM signal*

Equation 2.19 can be implemented as follows (Fig 2.4).



Method for generating narrowband FM signal.

Ideally, an FM signal has a **constant envelope** and for the case of a sinusoidal modulating frequency  $f_m$ , the angle  $\theta_i(t)$  is also sinusoidal with the same frequency.

However the modulated signal produced by the narrowband modulator of Fig differs from this ideal condition in two fundamental respects:

- The envelope contains residue amplitude modulation and therefore varies with time.
- For a sinusoidal modulating the angle  $\theta_i(t)$  Contains harmonic distortion in the form of third and higher-order harmonic of the modulation frequency  $f_m$ .

However, if  $\beta$ (modulation index) is restricted to  $\beta \leq 0.3$  radians, the effect of residual AM and harmonic are limited to negligible levels.

Returning to equation 2.19(pp.127),

$$s(t) = A_c \cos(2\pi f_c t) - \beta A_c \sin(2\pi f_c t) \cdot \sin(2\pi f_m t)$$

↑  
Narrowband FM signal

$$s(t) = A_c \cos 2\pi f_c t + \frac{1}{2} \beta A_c \left[ \cos 2\pi(f_c + f_m)t - \cos 2\pi(f_c - f_m)t \right]$$

↑  
Narrowband FM signal

Consider an AM signal equation

$$s(t) = A_c \cos(2\pi f_c t) + \frac{MA_c}{2} \left[ \cos 2\pi(f_c + f_m)t + \cos 2\pi(f_c - f_m)t \right]$$

↑  
AM signal  
 $\mu$  - Modulation factor of AM

Comparing equation, we see that in the case of sinusoidal modulation, the Basic difference between an AM signal & a narrowband FM signal is that the algebraic sign of the lower side frequency in the narrowband FM is reversed.

Thus, a narrowband FM signal requires essentially the same transmission band width (i.e.  $2f_m$ ) as the AM signal.

## Wideband Frequency Modulation:

The FM signal itself is given by

$$s(t) = A_c \cos(2\pi f_c t + \beta \sin 2\pi f_m t)$$

We wish to determine the spectrum of the single tone FM signal above, for an arbitrary value of the modulation index  $\beta$ .

Assuming  $\beta > 1$  (wideband frequency modulation we may write the above FM signal as

$$s(t) = A_c [\cos \omega_c t \cdot \cos \beta \sin \omega_m t - \sin \omega_c t \cdot \sin(\beta \sin \omega_m t)]$$

- $S(t)$  is no periodic,  $f_c$  is an integral multiple of  $f_m$ .
- We assume that  $f_c$  is large enough compared to the bandwidth of the FM signal.

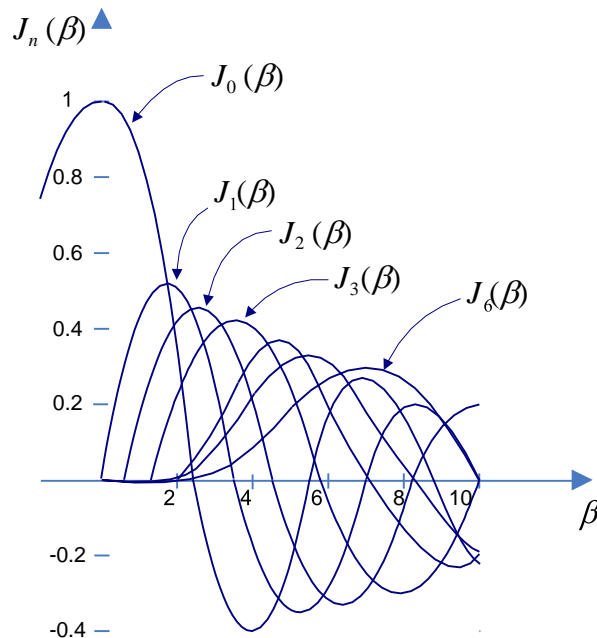
We know that:

$$\cos(\beta \sin \omega_m t) = J_0(\beta) + \sum_{n \text{ even}}^{\infty} 2J_n(\beta) \cos n \omega_m t$$

$$\sin(\beta \sin \omega_m t) = \sum_{n \text{ odd}}^{\infty} 2J_n(\beta) \sin n \omega_m t$$

Where  $n$  is positive and  $J_n(\beta)$  are coefficient of Bessel functions of the first kind, of order  $n$  argument  $\beta$ .

Figure below shows the Bessel function  $J_n(\beta)$  versus modulation index  $\beta$  for different positive integer value of  $n$ .



Bessel function for  $n=0$  to  $n=6$

We can develop further insight into the behavior of the Bessel function  $J_n(\beta)$ ,

(1)  $J_n(\beta) = (-1)^n J_{-n}(\beta)$  For all n both positive & negative.

(2) For small values of the modulation index  $\beta$ , we have

$$J_0(\beta) = 1$$

$$J_1(\beta) = \frac{\beta}{2}$$

$$J_n(\beta) = 0 \quad n > 2$$

(3)  $\sum_{n=-\infty}^{\infty} J_n^2(\beta) = 1$

Substituting equations and expanding products of sines and cosines finally yields:

$$s(t) = A_c J_0(\beta) \cos \omega_c t$$

$$+ \sum_{\substack{n \\ \text{odd}}}^{\infty} A_c J_n(\beta) [\cos(\omega_c + n \omega_m)t - \cos(\omega_c - n \omega_m)t]$$

$$+ \sum_{\substack{n \\ \text{even}}}^{\infty} A_c J_n(\beta) [\cos(\omega_c + n \omega_m)t + \cos(\omega_c - n \omega_m)t]$$

$$s(t) = A_c \sum_{n=-\infty}^{\infty} J_n(\beta) \cos(\omega_c + n \omega_m)t$$

↑

Wide-band FM

$s(t)$  is the desired form for the Fourier series representation of the single tone FM signal  $s(t)$  for an arbitrary value of  $\beta$ .

The discrete spectrum of  $s(t)$  is obtained by taking the Fourier transform of both sides of equation 2.15 & we have:

$$s(f) = \frac{A_c}{2} \sum_{n=-\infty}^{\infty} J_n(\beta) [\delta(f - (f_c + n f_m)) + \delta(f - (f_c - n f_m))]$$

↑

FM signal

From 2.15 & 2.16 we may make the following observation:

- (1) The spectrum of an FM signal contains a carrier component and an infinite set of side frequencies located symmetrically on either side of the carrier at frequency separations  $f_m, 2f_m, 3f_m, \dots$  (note in AM system a sinusoidal Modulating signal gives rise to only one pair of side frequencies).
- (2) For the special case of  $\beta$  small compared to unity, only the Bessel coefficients  $J_0(\beta)$  and  $J_1(\beta)$  have significant values, so that the FM signal is effectively

Composed of a carrier and a single pair of side frequency  $f_c \pm f_m$  at

This situation corresponds to the special case of narrowband FM that was considered earlier.

$$s(t) = \frac{AC}{2} J_0(\beta) [\cos(\omega_c t + \delta f t)] + \frac{AC}{2} J_1(\beta) [\cos(\omega_c t - \omega_m t + \delta f t) + \cos(\omega_c t + \omega_m t + \delta f t)]$$

$\uparrow$   
 $n=0$

$\uparrow$   
 $n=1$

[Note:  $J_0(\beta) = 1$ ,  $J_1(\beta) = \beta$ ]

